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Development of a Mathematical Model of the Electrical Properties of Bone

Thomas Wyss Balmer¹, Juan Ansó², Philippe Büchler¹, Andreas Stahel³

¹Institute for Surgical Technology and Biomechanics (ISTB), University of Bern;

²ARTORG Center for Biomedical Engineering, University of Bern;

³*Mathematics, Bern University of Applied Sciences*

Scope and Purpose Materials & M	d Purpose Materials & Methods		
Direct Cochlear Access (DCA) aims to replace mastoidectomy	Determination of the electrical properties of bone tissue [3].		
 Cochlear implants are successful hearing aids. 	 Evaluation and development of tools to measure bone properties in-vivo. 		
 Surgical procedure is complex and invasive. 	 Development of Electrical Impedance Spectroscopy signal protocol. 		
 Replace invasive mastoidectomy by minimal invasive drilling [1]. 	 Determine and minimize adverse influences on measurement system. 		
 No visual access to OP field 	 Impedance measurement of the sheep mastoid bone. 		
 Narrow drilling trajectory sets important nerves at risk 	 Development of measurement setup to in-vivo measure bone impedance in a 		
• Electromyography (EMG) has been proposed to assess drill to nerve distance [2].	sheep model		

- Current development lacks sensitivity and specificity.
- Bone electric properties required to improve safety.

 Apply electro impedance spectroscopy (EIS) sinusoidal waveforms with frequencies 15Hz, 110Hz and 1070Hz and current magnitudes of 125µA, 250µA and 500µA.



Amplitudes: 125µA, 250µA, 500µA Current is chosen below 500µA to not overstimulate the sheep's facial nerve.

Frequencies: 15Hz, 110Hz, 2070Hz 128 sine periods per frequency leads to a duration of approximately one minute signal time.

The multi electrode probes are manually inserted. Then the automatic protocol is started.



Figure 4: Two multi electrode probes a) inserted into mastoid of sheep model. The position of the main probe was recorded by the 3D navigation





Figure 5: The equivalent circuit used to model bone impedance was composed of a constant phase element (CPE) in series with R. CPE The resistor is symmetrically aligned at the contact phase where the steel electrode touches the bone tissue. This model allows to separate the real resistance of the bone from the hardly controllable phase shift introduced by the contact phase.



Figure 6: The scatterplot relates the product of bone density and inter-electrode distance $(D_N L)$ calculated from the model resistance R with D_N^*L of the tunnel where the current flows between the electrodes... Analysis of the resistance with the calculated simplified circuit showed a strong correlation of this resistance with, D_N*L whereby the correlation $(r^2=0.75)$ is best for the



Discussion

The impedance measured in-vivo could be described by a simple electronic circuit composed of a resistor in series with a constant phase element. Interestingly, the same set of parameters could be used to describe the behavior of the constant phase element for all the experimental measurements. This result indicate that the phase shift observed in the experimental impedance could be explained by the impedance at the bone/electrode interface caused by the **polarization of steel** The interface between the electrodes. electrodes and the body fluids is similar for all the measurement configuration and does not depend on the inter-electrode distance nor on the bone density. Therefore, our results support the hypothesis that the constant phase element describes the constant polarization and electrochemical processes happening at the bone/electrode interface. On the other hand, the resistor component of the circuit differs for each measurement. This resistance showed a high dependence to the average bone quality and inter-electrode distance, which corresponds to the representation of bone tissue as a perfect resistor. In addition, the model can be used to **predict the complex** impedance of the bone based on preoperative imaging – to determine the average bone density – and the measurement distance.

system of the robot b). a counter probe c) was applied to measure impedance. Fiducial screws to determine position of the mastoid d).

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- [2] J. Ansó, C. Stahl, N. Gerber, T. Williamson, K. Gavaghan, M. Caversaccio, S. Weber, and B. Bell, "Feasibility of Using EMG for Early Detection of the Facial Nerve During Robotic Direct Cochlear Access."
- [3] J. Sierpowska, J. T yr s, M. A. Hakulinen, S. Saarakkala, J. S. Jurvelin, R. Lappalainen, and J. Töyräs, "Electrical and dielectric properties of bovine trabecular bone--relationships with mechanical properties and mineral density.," *Phys. Med. Biol.*, vol. 48, no. 6, pp. 775–86, Mar. 2003.

Parameter	STD [%]	confidence interv
experimental data at 1060 Hz.(Table2).		

ρ = 14.3±2.1Ωm	14.4 %	10.1 Ωm – 18.5Ωm		
$Q_0 = 2.70 \ 10^{-5} \pm 0.8 \ 10^{-5}$	29.3 %	1.1 10 ⁻⁵ – 4.3 10 ⁻⁵		
n = 0.47 ± 0.06	13.5%	0.34 - 0.60		
ab1: Properties of equivalent circuit (Figure 5) determined by poplineer least				

Tab1: Properties of equivalent circuit (Figure 5) determined by nonlinear least mean square fitting.

Frequency	15 Hz	110 Hz	1060 Hz	All
Error Magnitudes Difference	15.7 %	20.8 %	24.6 %	20.4 %
Exp Data AVG re/im	4.04 kΩ/2.96 kΩ	2.40 kΩ/1.11 kΩ	1.70 kΩ/542 Ω	
STD / % of Exp AVG Real	622 Ω / 15.7 %	75 Ω / 3.21 %	16 Ω / 0.80 %	6.58 %
STD / % of Exp AVG Imag	1.08k Ω / 36.1 %	150 Ω / 12.2 %	40 Ω / 7.83 %	18.7 %
STD / % of Exp AVG	1.25k Ω / 24.9 %	174 Ω / 6.50 %	45.1 Ω / 2.54 %	11.3 %
Correlation DnL model	0.24	0.60	0.75	
to DnL experiment				

Tab2: Error to the model, average values and standard deviation of the experimental data. The relative error of the model impedance to the measured impedance overall is about 20 %...